

Measurement of PVT Data for Molten Potassium Chloride to 1320 K and 6 kbar

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(Z. Naturforsch. 31a, 656-663 [1976]; received April 13, 1976)

PVT data of molten KCl as a typical example for an ionic melt have been measured between 770 and 1050 °C at pressures up to 6 kbar. The experiments were performed in an internally heated pressure vessel containing argon as pressure transmitting medium. The salt was enclosed in a stainless steel cell the volume of which could be varied by means of a metal bellows and measured by monitoring the displacement of one end of the cell using an inductive transducer. The accuracy of the density data obtained is 0.15% for pressures below 2 kbar and 0.4% for higher pressures.

1. Introduction

Molten alkali halides are considered to be the simplest molten salts because they consist of only two different types of monovalent spherical ions. Therefore, the first computer simulation calculations on molten salts by the Monte Carlo¹ and the molecular dynamics² methods have been performed on the alkali halides, especially on potassium chloride. One purpose of these computer simulations is to calculate the macroscopic properties of ionic liquids and their temperature and density dependences from suitable pair potentials, since this cannot yet be done by rigorous statistical mechanical methods.

In order to test the validity of the results of such computer calculations a comparison with experimental data is necessary. Extensive experimental work has been done on the alkali halides at ordinary pressure, whereas an almost complete lack of information is existing for the high-pressure range. So far, only conductivity measurements up to 1 kbar have been published by Cleaver et al.³. Measurement of the PVT data over a wide range of temperature and pressure for molten potassium chloride as a first example of an ionic melt can provide valuable information, because they enable:

1. the derivation of an equation of state for a melt with long range forces between the constituent particles,
2. a comparison of the thermodynamic properties calculated from the equation of state with the properties of other types of liquids,

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3. a discussion of the properties of molten KCl, e.g. the electrical conductivity, which have been measured as a function of pressure and temperature in terms of density or average particle distance,
4. a test of the results of computer calculations at high pressures or high densities.

The experimental effort necessary is outlined by the following facts:

1. in order to allow for a 15% isothermal density change a pressure range of about 6 kbar is necessary,
2. at that pressure the melting temperature of KCl is almost 900 °C; consequently the temperature range of the experiments should exceed 1000 °C,
3. under those conditions of temperature and pressure the alkali halides are highly corrosive,
4. in order to be useful for the purposes mentioned above the accuracy of the densities should be about 0.5% or even better.

One experimental method suitable to match all those requirements utilizes as a volumeter a closed all-metal container the volume of which is variable by means of a metal bellows mounted in an internally heated pressure vessel.

2. Experimental

2.1 Pressure System

The pressure apparatus consists essentially of an internally heated pressure vessel and the pressure generating and measuring equipment. The inner cylinder of the composite pressure vessel which is shown schematically in Fig. 1 has an inner diameter of 60 mm and is made of maraging steel (Suprafort 200, Krupp). For the outer cylinder a heat-treatable

high strength steel is chosen. The outer surface of the pressure vessel is equipped with a water cooling system to keep the wall of the vessel at low temperatures. The bore of the pressure vessel is closed by Bridgman seals at either end.

The internal furnace (Fig. 2) consists of four independently controlled resistance heaters made of molybdenum wire insulated by thin-walled alumina tubes. Between the furnace and the wall of the pressure vessel zirconia, fired, and unfired pyrophyllite tubings are inserted for thermal insulation purposes. In order to avoid convection in the pressure transmitting compressed argon the insulating tubes fit smoothly and the gaps between them are sealed by O-rings at the upper end. In addition all cavities are filled carefully with alumina powder. The complete furnace is connected to the lower Bridgman plug through which the electrical leads enter the high-pressure chamber. Small electrically insulated Bridgman plugs made from copper-beryllium bronze which are positioned in inclined bores in the lower Bridgman plug serve as feed-throughs for the power leads.

The temperature is measured by three sheathed chromel-alumel thermocouples distributed along the volumometer. They enter the pressure vessel at a

position indicated in Fig. 1 through small Bridgman plugs into which they are soldered. The thermocouples are calibrated at the melting points of antimony and silver according to the International Practical Temperature Scale of 1968 (Sb: 630.74 °C; Ag: 961.93 °C) and at the melting point of KCl for which the value $T_F = 770.3$ °C of Roberts⁴ is chosen which was confirmed by Johnson and Bredig⁵ and was used in recent studies^{6, 7}.

The accuracy of temperature measurement including errors caused by temperature inhomogeneities is ± 2 K.

The vessel is pressurized by compressed argon. A two-stage diaphragm gas compressor (Nova) compresses argon from commercial cylinder supplies into the pressure vessel through the upper Bridgman

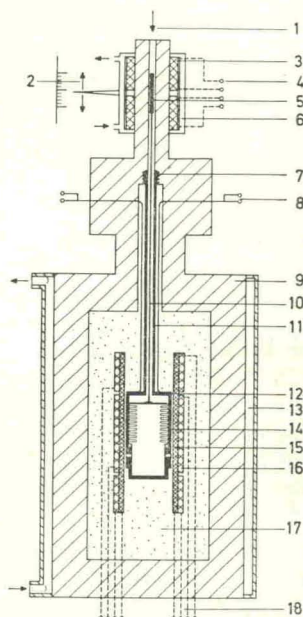


Fig. 1. Schematic diagram of high pressure apparatus: 1 gas inlet; 2 micrometer screw; 3 differential transformer; 4 leads to carrier frequency amplifier; 5 ferromagnetic tip; 6 thermostat; 7 fixed point of suspension system; 8 thermocouple inlets; 9 pressure vessel; 10 wire; 11 suspension tubing; 12 bracket; 13 cooling jacket; 14 volumometer with bellows; 15 main heater; 16 auxiliary heaters; 17 thermal insulation; 18 power leads.

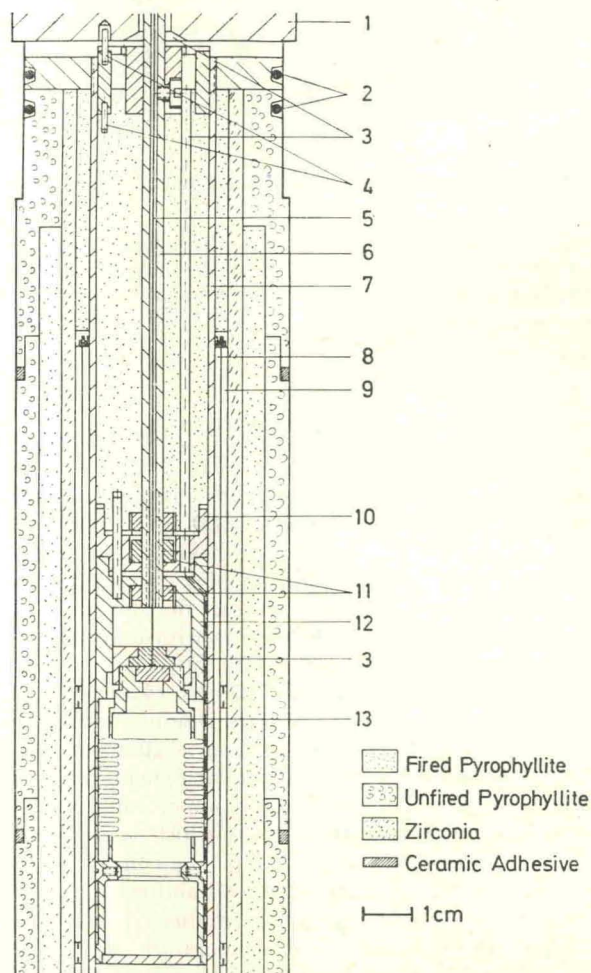


Fig. 2. Volumometer, heaters, and insulation: 1 upper Bridgman plug; 2 O-rings; 3 thermocouples; 4 anti-torsion pins; 5 wire; 6 suspension tubing; 7 inner tube of furnace; 8 main heater; 9 auxiliary heaters; 10 centering device; 11 nuts; 12 bracket; 13 volumometer with bellows.

plug and into a pressure intensifier (Autoclave Engineers) to pressures of 3000 bar. Higher pressures are generated by the intensifier operated by an air-driven hydraulic pump.

The gas pressure is measured by a set of Bourdon gauges (Heise) with ranges of 1000, 3000, and 7000 bar and an accuracy of 0.1% of full scale reading. The gauges are calibrated against a dead-weight tester.

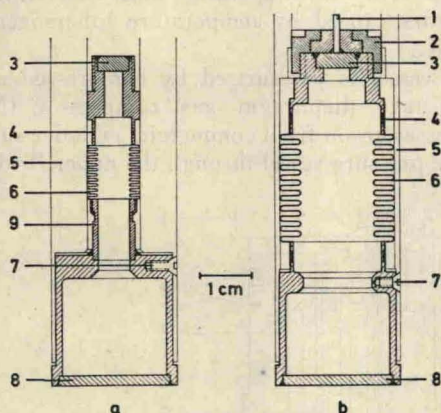


Fig. 3. Volumeters for different density ranges: a) type 1 for low densities, b) type 2 for high densities. 1 wire for displacement measurement; 2 gland; 3 lid (argon welded); 4 welded seam; 5 bracket; 6 metal bellows; 7 screw; 8 bottom part; 9 spacer.

2.2 Volumometer

The volumometer shown in Fig. 3 is a closed system of fixed salt content consisting of a rigid stainless steel cell (Remanit 1880 SST, Deutsche Edelstahl-Werke) and a metal bellows (material: Inconel 600, Henry Wiggin and Co.) which allows for pressure equilibration between the salt and the pressurizing argon. Metal bellows with different diameters are used depending on the density range leading to volumes between 7.2 and 14.3 cm³. The lower end of the volumometer is rigidly attached to a bracket which is suspended from a stainless steel tubing connected to the upper Bridgman plug as indicated in Figure 1. To the upper end of the volumometer a wire is attached which is made of the same material as the tubing, thus compensating for most of the thermal expansion and compression effects along the temperature gradient from measuring temperature to room temperature and in the upper Bridgman seal. The wire is carrying a ferromagnetic tip. Hence changes in volume of the volumometer can be measured via displacements of its upper end by a thermostatted differential transformer outside the high-pressure system which can be

moved up and down by a micrometer screw to find the relative zero position with respect to the ferromagnetic tip, which is monitored by a carrier frequency amplifier (Hottinger Meßtechnik). With this experimental set-up it is also possible to carry out quasi-isochoric measurements by adjusting the pressure in a way that the upper end of the volumometer is kept at the same (zero-)position when the salt is heated or cooled slowly.

Since the suspension system described above does not compensate for all expansion and compression effects completely, the small resultant erroneous zero point shift of the arrangement is determined by replacing the volumeter by a solid piece of metal of the same material and size and then measuring the movement of the ferromagnetic tip as a function of pressure and temperature. The resultant shift which is found to be reproducible to ± 0.07 mm with an additional uncertainty of 0.07 mm for the zero point position is taken into account as a correction to the displacements measured. The uncertainty in the final density values caused by this effect is only small for volumeters of type 1, but it is appreciable (0.25%) for type 2 volumeters. In this case it can be diminished by finding the zero point position with the aid of density values obtained with type 1 volumeters (see also Sect. 2.4 and Table 1).

2.3 Experimental Procedure

The zero point volume at 20 °C of the volumometer is determined before an experiment by differential weighing with water and carbon tetrachloride. The salt (E. Merck and Co., >99.5%) is dried carefully under vacuum at about 450 °C for at least six hours⁸, then fused in a quartz glass funnel and introduced into the volumometer. After filling and cooling down the volumometer the amount of salt is determined by differential weighing. Then the volumometer is closed by welding under dry argon gas and placed into the pressure vessel.

For densities smaller than the density of the fused salt at its melting point at 1 bar pressure cells of type 1 (Fig. 3) are used. They are heated at ordinary pressure until the salt fills the zero point volume of the volumometer completely. Upon further heating the pressure is adjusted in a way, that a quasi-isochoric measurement can be performed. For densities higher than the density of the liquid at its ordinary melting point volumeters of type 2 are chosen because the larger bellows allow for the volume increase of the salt upon fusion without irreversible deformations caused by large elongations. In order to check the consistency of the isochores in this range additional isothermal mea-

measurements are made. For this purpose the volume of the volumeters is calibrated as a function of the displacement of its upper end using density values obtained by isochoric measurements. It turns out that for volume changes smaller than about $\pm 15\%$ even under these extreme conditions the volume-displacement relation is reproducible although not linear, as was also observed by Babb et al.⁹ at room temperature. If the volume change of the bellows caused by melting of the salt at 1 bar exceeds about 15% it may be partly irreversible. In this case a redetermination of the zero point volume of the bellows and of its cross-section is necessary with the aid of density values determined with volumeters of type 1. This leads to an additional uncertainty in the final density values of about 0.15% (see also Sect. 2.4 and Table 1).

2.4 Determination of Density

The density of molten KCl corresponding to a measured pair of temperature and pressure is calculated from

$$\rho(P, T) = m/V_0(P, T) = m/[V_0(1 \text{ bar}, 20^\circ\text{C}) + \Delta V_{T,C} + \Delta V_{T,B} + \Delta V_P] \quad (1)$$

where m is the amount of salt in the volumeter, $V_0(P, T)$ the volume of the volumeter at P and T and zero displacement, $V_0(1 \text{ bar}, 20^\circ\text{C})$ the calibrated volume at 1 bar and 20°C , $\Delta V_{T,C}$ the volume correction of the total volumeter due to thermal expansion as if it were totally made from the material of the rigid part. $\Delta V_{T,B}$ a correction to $\Delta V_{T,C}$ taking into account, that the bellows and the rigid part are made from different materials, ΔV_P the correction due to compression of the volumeter. All the corrections are temperature and pressure dependent.

The corrections due to thermal expansion are calculated according to

$$\Delta V_{T,C} = 3 V_0(1 \text{ bar}, 20^\circ\text{C}) \alpha_C [t - 20], \quad (2)$$

$$\Delta V_{T,B} = -2 V_{0,B}(1 \text{ bar}, 20^\circ\text{C}) \Delta \alpha_{C-B} [t - 20], \quad (3)$$

where α is the average linear thermal expansion coefficient between 20°C and the measuring temperature, $\Delta \alpha_{C-B} = \alpha_C - \alpha_B$ is the difference between the coefficients for cell and bellows materials, t is the measuring temperature in degrees centigrade, and $V_{0,B}(1 \text{ bar}, 20^\circ\text{C})$ is the volume of the bellows at 1 bar, 20°C , and zero displacement. Equation (3) is taking into account that the correction for the

difference in thermal expansion between the cell and bellows materials in axial direction is already included in the displacement measurement.

The values used for the different thermal expansion coefficients in the range between 800 and 1050°C are.

$$\alpha_C = (16.4 + 0.003 t \pm 0.3) \cdot 10^{-6} \text{ (see } 10\text{)},$$

$$\alpha_B = (12.9 + 0.004 t) \cdot 10^{-6} \text{ (see } 11\text{)},$$

$$\Delta \alpha_{C-B} = (3.5 - 0.001 t) \cdot 10^{-6}.$$

The relative uncertainty of α_C amounts to 1.6%, that of $\Delta \alpha_{C-B}$ is estimated to be 8%. The corresponding errors in $V_0(P, T)$ are 0.09% and 0.02%, respectively. The pressure dependence of the thermal expansion coefficient is small and can therefore be neglected in the thermal expansion correction.

Since the overall correction for the compression of the volumeter is of the order 0.5% in $V_0(P, T)$, it is not necessary to distinguish between the compressibilities of the two different materials and to take into account the pressure dependence of the compressibility when calculating the correction which can then be written as

$$\Delta V_P = -\beta(T) P [V_0(1 \text{ bar}, 20^\circ\text{C}) + \Delta V_{T,C} + \Delta V_{T,B}]. \quad (4)$$

The compressibility $\beta(T)$ may be calculated from

$$\beta(T) = \frac{3[1 - 2\nu(T)]}{E(T)} \quad (5)$$

with data for Young's modulus $E(T)$ ¹² and Poisson's ratio $\nu(T)$ ¹³ extrapolated beyond 820°C . It turns out that ν does not show a systematic variation with temperature. It thus has its usual value $\nu = 0.3$ over the whole temperature range. For $E(T)$ the following relation holds:

$$E(T) = 22860 - 11.6 t \text{ (in } \text{kp mm}^{-2}\text{)}.$$

The value for β at room temperature obtained from Eq. (5) is $6.02 \cdot 10^{-7} \text{ bar}^{-1}$. It is in good agreement with data for the constituent pure metals obtained by Bridgman¹⁴ from high-pressure experiments. He also demonstrated that the pressure dependence of the compressibility may be expressed as a linear function of pressure and that the pressure dependent term is contributing less than 5% below 6 kbar. Hence it is justified to neglect it here.

The estimated error of the compressibility is about 10% below 2 kbar and about 20% for the highest pressures. This leads to errors in $V_0(P, T)$ of 0.025% and 0.13%, respectively.

2.4 Uncertainties in Density

The uncertainties in the final density values caused by various experimental errors may be obtained from

$$\begin{aligned} \Delta\rho/\rho = & \Delta m/m + [\Delta V_0(1 \text{ bar}, 20^\circ\text{C}) + \Delta V_0(P, T) \\ & + q_0(\Delta l - \Delta l_0) + \Delta V_{\text{cal}}]/V_0(P, T) \quad (6) \\ & + \alpha \Delta T + \beta \Delta P \end{aligned}$$

where the symbols appearing for the first time have the following significance: Δm : error in the amount of salt in the volumometer, $\Delta V_0(1 \text{ bar}, 20^\circ\text{C})$: error in volume calibration; $\Delta V_0(P, T)$: error due to inaccuracies of the corrections $\Delta V_{T,C}$, $\Delta V_{T,B}$, and ΔV_P ; Δl : uncertainty in displacement measurement; Δl_0 : reduction of Δl by fixing the zero point of displacement for type 2 volumometers by calibration (see Sect. 2.2); ΔV_{cal} : uncertainty in calibration of $V_0(P, T)$ and q_0 of type 2 volumometers after an irreversible volume change (see Sect. 2.3); ΔT , ΔP : errors in temperature and pressure measurement, respectively (see Sect. 2.1); α , β : thermal expansion coefficient and isothermal compressibility of the salt, respectively.

The numerical values of the uncertainties for the two different types of volumometers are given in Table 1 for various pressures.

Table 1. Relative uncertainties of final density value due to various experimental errors.

| Volumometers Pressure | Type 1 | | Type 2 |
|---|--------|----------|----------|
| | 1 bar | 2000 bar | 6000 bar |
| $\Delta m/m$ | 0.017 | 0.017 | 0.008 |
| $\Delta V_0(1 \text{ bar}, 20^\circ\text{C})/V_0(P, T)$ | 0.035 | 0.035 | 0.042 |
| $\Delta V_0(P, T)/V_0(P, T)$ | 0.090 | 0.115 | 0.240 |
| $q_0 \Delta l/V_0(P, T)$ | 0.050 | 0.080 | 0.250 |
| $q_0 \Delta l_0/V_0(P, T)$ | — | — | -0.150 |
| $\Delta V_{\text{cal}}/V_0(P, T)$ | — | — | 0.150 |
| $\alpha \Delta T$ | 0.085 | 0.062 | 0.041 |
| $\beta \Delta P$ | 0.006 | 0.009 | 0.012 |
| total $\Delta\rho/\rho$ | 0.28 | 0.32 | 0.59 |
| $\Delta\rho/\rho$ when based on values at 1 bar | 0.1 | 0.14 | 0.41 |

3. Results

Following the procedure described above twenty quasi-isochores with 431 experimental points and nine isotherms with 87 points are measured covering

the temperature, pressure, and density ranges from 770 to 1050 °C, from 1 to 6000 bar, and from 1.36 to 1.67 g cm⁻³, respectively. The uncorrected points of some of the quasi-isochores are shown in Fig. 4, where the points obtained upon heating and cooling in different cycles are marked by different symbols. As may be seen from the figure, the scatter of the experimental points is very small and statistical, thus indicating that there is neither hysteresis nor any time-dependent effect.

All unsmoothed experimental points corrected for the effects described in Sects. 2.2 and 2.4 are collected in Table 2.

Since PVT data for molten KCl at high pressures have not been published previously, a comparison with data from other sources is not feasible. Density values at normal pressure obtained by fitting a second order polynomial to the quasi-isochores shown in Fig. 4, subsequent numerical extrapolation of $T(P)$ to normal pressure and calculating the corresponding density values from Eq. (1) are shown

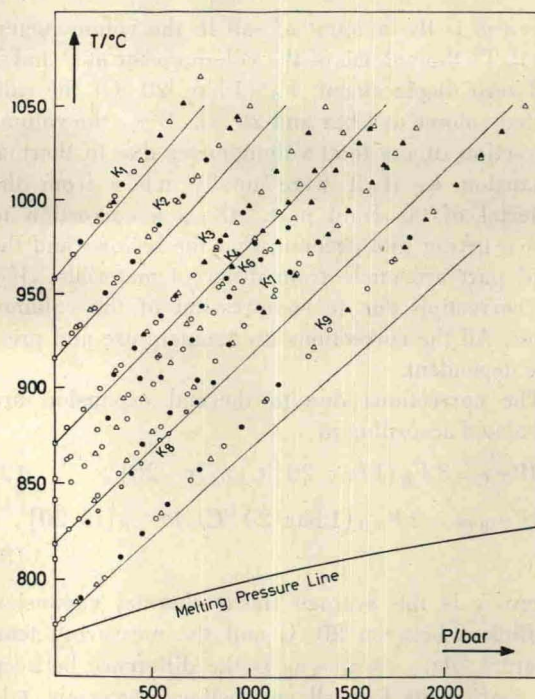


Fig. 4. Uncorrected experimental points on quasi-isochores and isochores (full lines) corresponding to quasi-isochores K_1 , K_2 , K_3 , K_7 , and K_9 . ● heating first run, ○ cooling first run, △ heating second run, ▲ cooling second run, □ extrapolated points at 1 bar (see text).

Table 2. Unsmoothed corrected experimental points for density determinations of molten potassium chloride.

| P/bar | T/°C | ρ/gcm^{-3} | P/bar | T/°C | ρ/gcm^{-3} | P/bar | T/°C | ρ/gcm^{-3} | P/bar | T/°C | ρ/gcm^{-3} |
|-------|--------|------------------------|-------|--------|------------------------|-------|--------|------------------------|-------|--------|------------------------|
| 1 | 958.2 | 1.4180 | 485 | 980.0 | 1.4379 | 877 | 981.0 | 1.4606 | 526 | 911.5 | 1.4772 |
| 136 | 978.0 | 1.4166 | 631 | 1000.0 | 1.4363 | 768 | 967.0 | 1.4616 | 684 | 930.0 | 1.4758 |
| 244 | 992.5 | 1.4155 | 733 | 1013.5 | 1.4353 | 625 | 949.5 | 1.4630 | 950 | 963.5 | 1.4731 |
| 348 | 1008.5 | 1.4143 | 846 | 1029.0 | 1.4340 | 460 | 929.0 | 1.4646 | 1119 | 983.5 | 1.4714 |
| 476 | 1025.5 | 1.4130 | 943 | 1042.5 | 1.4329 | 1 | 852.3 | 1.4797 | 1334 | 1010.5 | 1.4692 |
| 897 | 1038.5 | 1.4138 | 824 | 1044.5 | 1.4321 | 274 | 899.0 | 1.4775 | 1206 | 995.0 | 1.4705 |
| 308 | 1002.0 | 1.4148 | 1006 | 1050.0 | 1.4323 | 441 | 905.5 | 1.4759 | 1058 | 977.5 | 1.4719 |
| 218 | 988.5 | 1.4158 | 899 | 1038.5 | 1.4332 | 596 | 924.0 | 1.4744 | 915 | 960.0 | 1.4733 |
| 96 | 971.0 | 1.4171 | 1 | 870.9 | 1.4689 | 752 | 943.5 | 1.4729 | 773 | 941.5 | 1.4749 |
| 278 | 997.0 | 1.4152 | 157 | 889.0 | 1.4676 | 882 | 958.5 | 1.4717 | 620 | 922.0 | 1.4764 |
| 447 | 1021.0 | 1.4134 | 304 | 907.0 | 1.4663 | 1028 | 977.0 | 1.4702 | 508 | 909.5 | 1.4774 |
| 589 | 1041.5 | 1.4118 | 413 | 921.5 | 1.4652 | 840 | 953.5 | 1.4721 | 394 | 895.5 | 1.4785 |
| 750 | 1065.5 | 1.4099 | 546 | 938.5 | 1.4639 | 701 | 936.5 | 1.4734 | 287 | 882.5 | 1.4794 |
| 659 | 1051.5 | 1.4110 | 852 | 978.0 | 1.4608 | 530 | 916.5 | 1.4750 | 186 | 870.5 | 1.4803 |
| 541 | 1034.0 | 1.4124 | 970 | 994.0 | 1.4594 | 378 | 896.5 | 1.4766 | 112 | 862.0 | 1.4809 |
| 305 | 999.0 | 1.4151 | 830 | 975.0 | 1.4610 | 217 | 877.5 | 1.4780 | 73 | 857.5 | 1.4812 |
| 1 | 916.0 | 1.4426 | 710 | 960.0 | 1.4622 | 79 | 863.5 | 1.4789 | 41 | 854.5 | 1.4814 |
| 261 | 950.5 | 1.4401 | 611 | 947.5 | 1.4632 | 61 | 862.5 | 1.4790 | 1 | 841.5 | 1.4860 |
| 402 | 967.5 | 1.4389 | 518 | 934.5 | 1.4642 | 354 | 894.5 | 1.4767 | 550 | 906.0 | 1.4813 |
| 536 | 986.5 | 1.4374 | 342 | 912.0 | 1.4660 | 534 | 917.0 | 1.4750 | 710 | 926.0 | 1.4797 |
| 658 | 1002.5 | 1.4362 | 236 | 899.5 | 1.4659 | 679 | 934.0 | 1.4736 | 895 | 949.0 | 1.4776 |
| 779 | 1022.0 | 1.4346 | 147 | 888.5 | 1.4677 | 860 | 955.0 | 1.4720 | 1058 | 968.0 | 1.4763 |
| 708 | 1010.5 | 1.4355 | 63 | 879.0 | 1.4683 | 1027 | 979.5 | 1.4699 | 1201 | 986.0 | 1.4748 |
| 622 | 1000.5 | 1.4363 | 313 | 909.0 | 1.4662 | 1156 | 994.0 | 1.4687 | 1106 | 974.0 | 1.4758 |
| 509 | 984.0 | 1.4376 | 473 | 930.0 | 1.4646 | 1265 | 1009.0 | 1.4675 | 964 | 957.0 | 1.4772 |
| 425 | 972.5 | 1.4385 | 638 | 950.0 | 1.4630 | 1486 | 1036.0 | 1.4652 | 815 | 940.0 | 1.4786 |
| 247 | 958.5 | 1.4395 | 824 | 973.5 | 1.4613 | 1338 | 1016.0 | 1.4669 | 660 | 921.0 | 1.4801 |
| 205 | 942.5 | 1.4407 | 935 | 988.0 | 1.4599 | 1203 | 995.5 | 1.4683 | 510 | 902.5 | 1.4816 |
| 131 | 933.5 | 1.4413 | 1066 | 1005.5 | 1.4585 | 1067 | 983.5 | 1.4696 | 373 | 884.0 | 1.4830 |
| 90 | 929.0 | 1.4417 | 1220 | 1026.0 | 1.4568 | 912 | 964.0 | 1.4712 | 247 | 869.0 | 1.4841 |
| 49 | 923.5 | 1.4420 | 1393 | 1049.5 | 1.4548 | 1 | 848.7 | 1.4818 | 154 | 859.0 | 1.4848 |
| 109 | 932.5 | 1.4414 | 1305 | 1036.0 | 1.4560 | 106 | 862.0 | 1.4809 | 83 | 850.5 | 1.4854 |
| 183 | 941.5 | 1.4408 | 1142 | 1015.5 | 1.4577 | 245 | 878.0 | 1.4798 | 209 | 865.0 | 1.4844 |
| 302 | 956.0 | 1.4397 | 1000 | 997.0 | 1.4592 | 410 | 897.5 | 1.4783 | 317 | 879.0 | 1.4834 |
| 448 | 984.0 | 1.4822 | 1313 | 971.5 | 1.4874 | 702 | 851.5 | 1.5184 | 1125 | 906.5 | 1.5110 |
| 600 | 913.5 | 1.4807 | 1450 | 987.0 | 1.4861 | 522 | 831.5 | 1.5200 | 1288 | 925.0 | 1.5095 |
| 748 | 931.5 | 1.4793 | 1600 | 1005.5 | 1.4845 | 257 | 801.0 | 1.5223 | 1161 | 910.0 | 1.5107 |
| 919 | 952.5 | 1.4775 | 1749 | 1025.0 | 1.4829 | 42 | 779.5 | 1.5238 | 1042 | 895.0 | 1.5122 |
| 1088 | 972.5 | 1.4759 | 1858 | 1038.5 | 1.4818 | 108 | 787.0 | 1.5232 | 905 | 879.5 | 1.5134 |
| 1230 | 991.0 | 1.4744 | 1790 | 1031.0 | 1.4824 | 212 | 797.5 | 1.5225 | 1294 | 879.0 | 1.5328 |
| 1380 | 1008.5 | 1.4729 | 1696 | 1019.0 | 1.4834 | 547 | 834.5 | 1.5175 | 1156 | 863.5 | 1.5341 |
| 1513 | 1024.0 | 1.4716 | 1705 | 1018.0 | 1.4835 | 803 | 862.5 | 1.5175 | 1005 | 847.0 | 1.5357 |
| 1639 | 1039.5 | 1.4703 | 1632 | 1010.0 | 1.4841 | 1078 | 893.0 | 1.5150 | 864 | 830.0 | 1.5371 |
| 1620 | 1038.0 | 1.4705 | 1510 | 995.0 | 1.4854 | 1329 | 921.5 | 1.5126 | 719 | 813.5 | 1.5381 |
| 1561 | 1030.5 | 1.4711 | 1404 | 982.0 | 1.4865 | 1510 | 943.0 | 1.5107 | 555 | 795.5 | 1.5386 |
| 1447 | 1016.0 | 1.4723 | 1235 | 960.0 | 1.4883 | 1736 | 968.5 | 1.5086 | 659 | 809.0 | 1.5381 |
| 1439 | 1015.5 | 1.4723 | 1072 | 940.5 | 1.4900 | 1950 | 994.5 | 1.5064 | 807 | 826.0 | 1.5373 |
| 1317 | 999.5 | 1.4737 | 1 | 811.0 | 1.5038 | 2195 | 1023.5 | 1.5041 | 951 | 841.5 | 1.5361 |
| 1146 | 977.5 | 1.4755 | 171 | 829.5 | 1.5025 | 2426 | 1050.5 | 1.5021 | 1099 | 857.5 | 1.5346 |
| 1 | 818.7 | 1.4993 | 393 | 854.5 | 1.5007 | 2300 | 1037.0 | 1.5031 | 1243 | 873.5 | 1.5333 |
| 449 | 870.0 | 1.4956 | 585 | 875.5 | 1.4991 | 2196 | 1025.0 | 1.5040 | 1411 | 893.5 | 1.5311 |
| 593 | 887.0 | 1.4943 | 730 | 892.5 | 1.4977 | 2087 | 1009.0 | 1.5053 | 1564 | 910.5 | 1.5291 |
| 736 | 904.5 | 1.4929 | 816 | 903.0 | 1.4969 | 1910 | 990.5 | 1.5068 | 1663 | 920.5 | 1.5281 |
| 894 | 923.5 | 1.4913 | 682 | 887.5 | 1.4981 | 1799 | 975.5 | 1.5080 | 1824 | 940.5 | 1.5259 |
| 1049 | 942.5 | 1.4898 | 542 | 872.5 | 1.4993 | 1504 | 942.0 | 1.5108 | 1989 | 960.5 | 1.5237 |
| 1205 | 961.5 | 1.4882 | 443 | 860.0 | 1.5003 | 180 | 811.5 | 1.5137 | 2177 | 983.0 | 1.5215 |
| 1354 | 978.0 | 1.4868 | 343 | 848.0 | 1.5012 | 292 | 820.5 | 1.5148 | 2080 | 968.5 | 1.5229 |
| 1254 | 965.5 | 1.4878 | 223 | 835.5 | 1.5021 | 458 | 833.5 | 1.5153 | 1941 | 950.5 | 1.5249 |
| 1128 | 951.5 | 1.4890 | 1 | 776.5 | 1.5238 | 604 | 848.5 | 1.5150 | 1792 | 933.5 | 1.5267 |
| 973 | 933.0 | 1.4905 | 133 | 790.5 | 1.5230 | 773 | 867.0 | 1.5141 | 1477 | 879.0 | 1.5401 |
| 829 | 914.0 | 1.4921 | 338 | 812.0 | 1.5214 | 941 | 887.0 | 1.5128 | 1673 | 900.0 | 1.5381 |
| 686 | 897.0 | 1.4935 | 451 | 824.0 | 1.5205 | 855 | 875.5 | 1.5137 | 1647 | 916.5 | 1.5364 |
| 544 | 879.5 | 1.4949 | 577 | 839.0 | 1.5193 | 716 | 858.5 | 1.5148 | 1569 | 889.0 | 1.5391 |
| 421 | 866.0 | 1.4959 | 754 | 857.0 | 1.5179 | 568 | 842.0 | 1.5155 | 1383 | 870.0 | 1.5408 |
| 331 | 855.0 | 1.4968 | 961 | 879.5 | 1.5161 | 415 | 828.5 | 1.5156 | 1178 | 848.0 | 1.5428 |
| 222 | 843.0 | 1.4976 | 1152 | 902.0 | 1.5142 | 320 | 820.5 | 1.5156 | 967 | 825.0 | 1.5446 |
| 124 | 831.5 | 1.4985 | 1510 | 943.0 | 1.5107 | 205 | 810.5 | 1.5147 | 729 | 800.0 | 1.5464 |
| 72 | 826.0 | 1.4988 | 1826 | 980.0 | 1.5076 | 96 | 801.0 | 1.5139 | 1058 | 834.5 | 1.5439 |
| 201 | 840.5 | 1.4978 | 1732 | 968.0 | 1.5086 | 256 | 815.5 | 1.5146 | 1426 | 874.5 | 1.5405 |
| 370 | 861.5 | 1.4962 | 1607 | 953.0 | 1.5099 | 373 | 825.0 | 1.5153 | 1763 | 909.5 | 1.5372 |
| 502 | 876.5 | 1.4951 | 1445 | 931.5 | 1.5117 | 521 | 838.5 | 1.5155 | 1970 | 931.5 | 1.5351 |
| 715 | 900.5 | 1.4932 | 1298 | 917.5 | 1.5129 | 679 | 854.5 | 1.5144 | 2160 | 952.5 | 1.5329 |
| 914 | 923.5 | 1.4914 | 1088 | 894.0 | 1.5149 | 818 | 871.5 | 1.5140 | 2386 | 980.0 | 1.5304 |
| 1125 | 948.5 | 1.4893 | 872 | 869.5 | 1.5169 | 976 | 890.0 | 1.5125 | 2555 | 1000.5 | 1.5285 |
| 2776 | 1028.5 | 1.5263 | 2652 | 965.0 | 1.5493 | 2838 | 921.5 | 1.5741 | 4646 | 964.0 | 1.6153 |
| 2641 | 1009.5 | 1.5278 | 2873 | 925.5 | 1.5468 | 3071 | 947.5 | 1.5717 | 4567 | 955.5 | 1.6160 |
| 953 | 796.0 | 1.5580 | 3138 | 1025.5 | 1.5439 | 3287 | 971.0 | 1.5696 | 4389 | 935.5 | 1.6179 |
| 1104 | 813.0 | 1.5563 | 3286 | 1044.0 | 1.5422 | 3475 | 993.5 | 1.5675 | 4155 | 911.0 | 1.6202 |
| 1265 | 830.0 | 1.5549 | 3169 | 1027.0 | 1.5437 | 3671 | 1016.5 | 1.5654 | 4804 | 921.0 | 1.6352 |
| 1409 | 846.0 | 1.5530 | 3080 | 1017.0 | 1.5446 | 3953 | 1049.5 | 1.5625 | 4469 | 885.0 | 1.6386 |
| 1576 | 863.5 | 1.5510 | 2969 | 1002.0 | 1.5460 | 3817 | 1031.5 | 1.5641 | 4319 | 875.0 | 1.6396 |
| 1768 | 885.0 | 1.5487 | 2780 | 979.0 | 1.5480 | 3708 | 1018.0 | 1.5653 | 4583 | 899.0 | 1.6373 |
| 1585 | 863.5 | 1.5510 | 2585 | 954.5 | 1.5503 | 3573 | 1002.5 | 1.5667 | 4788 | 918.5 | 1.6354 |
| 1445 | 849.0 | 1.5528 | 2410 | 935.5 | 1.5520 | 3027 | 989.0 | 1.5689 | 4929 | 934.5 | 1.6339 |
| 1300 | 833.5 | 1.5543 | 2438 | 900.0 | 1.5681 | 3429 | 944.0 | 1.5847 | 5146 | 957.0 | 1.6318 |
| 1185 | 820.0 | 1.5557 | 2208 | 876.0 | 1.5704 | 3615 | 964.5 | 1.5828 | 5356 | 981.5 | 1.6295 |
| 1002 | 799.0 | 1.5577 | 1975 | 849.5 | 1.5728 | 3860 | 993.5 | 1.5802 | 5562 | 1003.5 | 1.6275 |
| 1000 | 799.0 | 1.5577 | 1723 | 822.5 | 1.5753 | 4064 | 1017.5 | 1.5780 | 5748 | 1023.5 | 1.6256 |
| 1143 | 815.0 | 1.5561 | 1847 | 837.5 | 1.5739 | 4208 | 1035.5 | 1.5764 | 6028 | 1055.5 | 1.6227 |
| 1336 | 836.0 | 1.5541 | 2025 | 856.5 | 1.5722 | 4081 | 1021.0 | 1.5777 | | | |
| 1506 | 856.5 | 1.5519 | 2164 | 871.5 | 1.5709 | 3948 | 1004.0 | 1.5792 | | | |
| 1685 | 877.5 | 1.5496 | 2359 | 893.5 | 1.5687 | 3744 | 980.5 | 1.5814 | | | |
| 1835 | 894.5 | 1.5476 | 2580 | 918.0 | 1.5665 | 3531 | 955.5 | 1.5837 | | | |
| 2007 | 913.5 | 1.5456 | 2769 | 938.5 | 1.5646 | 3320 | 931.5 | 1.5859 | | | |
| 1892 | 899.5 | 1.5470 | 2976 | 961.5 | 1.5625 | 3110 | 907.0 | 1.5882 | | | |
| 1720 | 881.5 | 1.5493 | 3174 | 985.0 | 1.5604 | 2900 | 884.0 | 1.5903 | | | |
| 1600 | 867.5 | 1.5507 | 3378 | 1007.5 | 1.5584 | 2668 | 858.5 | 1.5927 | | | |
| 1434 | 848.5 | 1.5528 | 3630 | 1038.0 | 1.5566 | 3637 | 920.0 | 1.6007 | | | |
| 1286 | 833.0 | 1.5544 | 3521 | 1024.0 | 1.5569 | 3443 | 899.5 | 1.6026 | | | |
| 1169 | 820.0 | 1.5557 | 3388 | 1008.0 | 1.5583 | 3252 | 879.0 | 1.6045 | | | |

in Fig. 5 in comparison with data from the literature¹⁵⁻²⁶ which show considerable discrepancies.

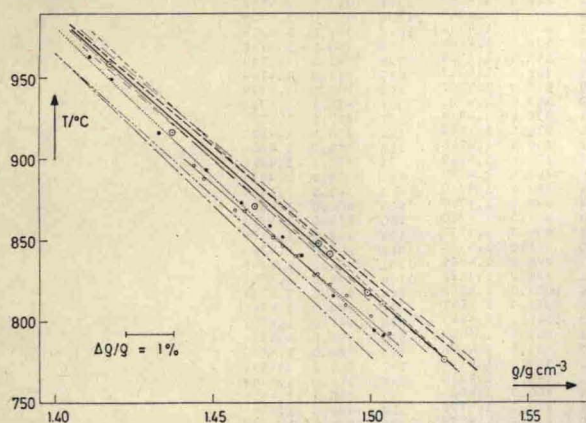


Fig. 5. Density of molten potassium chloride as a function of temperature at 1 bar. — Grjotheim et al. (1971)¹⁵, — Kirshenbaum et al. (1962)¹⁶, ●····· Neithamer and Peake (1961)¹⁷, — Van Artsdalen and Yaffe (1955)¹⁸, ○ Peake and Bothwell (1954)²⁰, - - - Bloom et al. (1953)²¹, - - - Mashovetz and Lundina (1935)²², - - - Klemm (1926)²³, - · - · - Jäger (1917)²⁵, - - - Brunner (1904)²⁶, ⊙ This work.

Our extrapolated values, with the exception of two, agree to better than 0.1% with the data of Van Artsdalen and Yaffe^{18, 19}. A linear fit of our extrapolated densities as a function of temperature is almost identical with that of Yaffe and Van Artsdalen¹⁹ and may be expressed as

$$\rho_0(T) = \rho_{0YA}(T) = 1.9767 - 0.5831 \cdot 10^{-3} t.$$

The good agreement with the accurate values of Van Artsdalen and Yaffe points out that our smoothed values at 1 bar pressure are accurate to about 0.1% rather than 0.28% as noted in the second last line of Table 1 and that the error limits of the high-pressure density values can be changed to the numbers given in the last line of Table 1, if the densities are based on the smoothed values at 1 bar rather than being regarded as absolute values.

The corrected experimental density values are fitted by an equation of state (modified Tait-equation) with temperature and pressure as independent variables with a standard deviation of 0.04% in density. The smoothed data are reported in Table 3.

Table 3. Smoothed density values in g/cm³ for molten potassium chloride.

| T/°C P/bar | 800 | 825 | 850 | 875 | 900 | 925 | 950 | 975 | 1000 | 1025 | 1050 |
|---------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 1 | 1.510 | 1.496 | 1.481 | 1.467 | 1.452 | 1.437 | 1.423 | 1.408 | 1.394 | 1.379 | 1.364 |
| 250 | 1.523 | 1.509 | 1.495 | 1.481 | 1.468 | 1.454 | 1.440 | 1.426 | 1.412 | 1.398 | 1.384 |
| 500 | 1.536 | 1.522 | 1.509 | 1.495 | 1.482 | 1.469 | 1.455 | 1.442 | 1.428 | 1.415 | 1.402 |
| 750 | 1.547 | 1.534 | 1.521 | 1.508 | 1.495 | 1.482 | 1.469 | 1.457 | 1.444 | 1.431 | 1.418 |
| 1000 | 1.558 | 1.546 | 1.533 | 1.520 | 1.508 | 1.495 | 1.483 | 1.470 | 1.458 | 1.445 | 1.432 |
| 1250 | | 1.556 | 1.544 | 1.532 | 1.519 | 1.507 | 1.495 | 1.483 | 1.471 | 1.459 | 1.446 |
| 1500 | | 1.566 | 1.554 | 1.542 | 1.530 | 1.519 | 1.507 | 1.495 | 1.483 | 1.471 | 1.459 |
| 1750 | | 1.576 | 1.564 | 1.552 | 1.541 | 1.529 | 1.518 | 1.506 | 1.495 | 1.483 | 1.472 |
| 2000 | | 1.585 | 1.573 | 1.562 | 1.551 | 1.540 | 1.529 | 1.517 | 1.506 | 1.495 | 1.483 |
| 2250 | | 1.594 | 1.583 | 1.572 | 1.561 | 1.550 | 1.540 | 1.528 | 1.518 | 1.506 | 1.495 |
| 2500 | | | 1.592 | 1.581 | 1.571 | 1.560 | 1.550 | 1.539 | 1.528 | 1.517 | 1.506 |
| 2750 | | | 1.600 | 1.590 | 1.580 | 1.569 | 1.559 | 1.548 | 1.538 | 1.527 | 1.517 |
| 3000 | | | 1.608 | 1.598 | 1.588 | 1.578 | 1.568 | 1.558 | 1.547 | 1.537 | 1.527 |
| 3250 | | | 1.616 | 1.606 | 1.596 | 1.587 | 1.577 | 1.567 | 1.557 | 1.547 | 1.536 |
| 3500 | | | 1.624 | 1.614 | 1.604 | 1.595 | 1.585 | 1.575 | 1.566 | 1.556 | 1.546 |
| 3750 | | | 1.631 | 1.622 | 1.612 | 1.603 | 1.593 | 1.584 | 1.574 | 1.564 | 1.555 |
| 4000 | | | 1.638 | 1.629 | 1.620 | 1.610 | 1.601 | 1.592 | 1.582 | 1.573 | 1.563 |
| 4250 | | | | 1.636 | 1.627 | 1.618 | 1.609 | 1.600 | 1.590 | 1.581 | 1.572 |
| 4500 | | | | 1.643 | 1.634 | 1.625 | 1.616 | 1.607 | 1.598 | 1.589 | 1.580 |
| 4750 | | | | 1.649 | 1.641 | 1.632 | 1.623 | 1.615 | 1.606 | 1.597 | 1.588 |
| 5000 | | | | 1.656 | 1.647 | 1.639 | 1.630 | 1.622 | 1.613 | 1.605 | 1.596 |
| 5250 | | | | 1.662 | 1.654 | 1.646 | 1.637 | 1.629 | 1.621 | 1.612 | 1.603 |
| 5500 | | | | 1.668 | 1.660 | 1.652 | 1.644 | 1.636 | 1.628 | 1.619 | 1.611 |
| 5750 | | | | | 1.666 | 1.659 | 1.651 | 1.643 | 1.634 | 1.626 | 1.618 |
| 6000 | | | | | 1.673 | 1.665 | 1.657 | 1.649 | 1.641 | 1.633 | 1.625 |

Smoothed isochores belonging to the uncorrected experimental points in Fig. 4 are shown as full lines in the same figure.

A discussion of the PVT data reported here, of the derivation of the equation of state used for fitting the results, and of some thermodynamic properties of molten potassium chloride calculated with

the aid of this equation will be published in a subsequent paper²⁷.

Acknowledgement

Financial support of this work by the Arbeitsgemeinschaft Industrieller Forschungsvereinigungen (AIF) from Funds of the Bundesministerium für Wirtschaft is gratefully acknowledged.

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